CEQA DRAINAGE STUDY

PIZZUTO PROPERTY COUNTY of SAN DIEGO TPM 20846/Log No. 04-08-030

Prepared for:

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Prepared by:

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> December 14, 2005 Revised September 8, 2006

> > W.O. 555-0915-400

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PURPOSE AND SCOPE:

The purpose of this report is to publish the results of hydrology and hydraulic computer analysis for the proposed Tentative Parcel Map for Pizzuto Property - County of San Diego TPM 20846. The proposed project is a 41.1-acre site and is proposed to be subdivided into 3 residential lots. The scope is to study the existing and proposed hydrology and hydraulics as it influences the surrounding properties during a 100-year frequency storm event.

PROJECT DESCRIPTION:

Pizzuto Property is located on Clayton Place, approximately 1600 feet north of the intersection between Deer Spring Place and Deer Spring Road. The nearest major road are Deer Spring Road and Highway 15. This 41.1 acres property is surrounded mostly by undeveloped land and rural used land. The site is steeply sloped and currently undeveloped.

The project proposes the subdividing the site into 3 residential lots, with each lot no less than 4 acres in size. The project proposes the grading of pads, driveways, and the improvement of Clayton Place and Deer Spring Place. In general, the pads will be graded on top of the topography and the pads will drained away from the pads and the runoff released into the existing drainage courses. There is an existing 18-inch culvert on Clayton Place (Node 3), just after the Deer Spring Place transition. This culvert is currently under sized and will be replaced with a proposed 24-inch pipe during the improvement of Clayton Place. The runoff that enters onto Deer Spring Place (Basin 5) is conveyed to the intersection of Deer Spring Place and Deer Spring Road via existing brow ditch along the easterly side of Deer Spring Place. The existing brow ditch will be replaced by the proposed curb and gutter when Deer Spring Place is improved. Because the elongation of the time of concentration due to the flattening of the terrain for the building pads, the increase in the peak runoff due to this development is minium (0.2 c.f.s. per acre in the worst case, for 4.2 acre basin). Since this project is still in the tentative map stage, no actual storm drain facilities have been design. Final placement and sizing of the storm drain facilities will be designed during the final engineering stage. No runoff will be released from this project that will cause harm to lives or properties. Runoff will be released into existing terrain below erosive velocity.

Due to the steepness of the existing terrain, erosion is always a concern. Currently, asphalt check dams are placed on the northern portion of Clayton Place. In the developed condition, the slopes will be landscaped and protected by brow ditches. The existing culvert will be redesigned so that the runoff will be released into the exist drainage course below the erosive velocity.

STUDY METHOD:

The method of analysis was based on the Rational Method according to the San Diego County Hydrology Manual. The Hydrology and Hydraulic Analysis were done on HydroSoft by Advanced Engineering Software.

Drainage basin areas were determined from the proposed grades shown on the Tentative Map for Pizzuto Property and 200-scale existing topographic maps from the County of San Diego.

The Rational Method provided the following variable coefficients:

Soil group C will be used for a composite runoff coefficient for the existing and proposed hydrology analyses.

The runoff coefficient for:

Existing Condition = Undisturbed Natural terrain = 0.30Proposed Condition = Low Density Residential (1 DU/A or less) = 0.36Rainfall Intensity = $I = 7.44x(P6)x(Tc)^0.645$

P6 for 100 year storm = 3.5

See Table 1.1 below comparison of existing and proposed storm drain flows.

Table 1.1 - Comparison of Existing and Proposed Storm Drain Flows

| Basin | Existing (cfs/ac) | Proposed (cfs/ac) |
|-------|-------------------|-------------------|
| 1 & 2 | 62.4/34.7 | 65.8/37.2 |
| 3 | 33.7/18.4 | 32.6/18.4 |
| 4 | 7.2/3.6 | 7.1/3.6 |
| 5 | 7.3/4.2 | 8.1/4.2 |

CONCLUSION:

The development of Pizzuto Property will disturbed approximately 3 acres of land or 10% of the total site. This project will change the land use from Natural Terrain to Low Density Residential-(1 du/a or less). Because this development proposes the flattening of the topography for the building pads, the time of concentration is elongated and the result is minimal increases in the peak runoff.

It was brought to our attention during the planning stage that this development have increased the peak runoff from Basin 1 & 2, (the peak runoff rate of 3.6 cfs for 34.7 acre

basin). However, with the new design, RPL #3, the time of concentration is prolonged and the peak runoff rate for Basin 1&2 has been reduced to the existing condition. Furthermore, from a field visit, the downstream channel that receives the runoff from node 14 (Basin 1 &2) is no less than 15 foot wide at its base. If there was an increase of 3.6 cfs than the water surface level would have been raised by approximately 0.2 feet.

Since, this project is still in it's tentative stage, no actual storm drain structure is being design at this point. Storm drain structure will be designed and sized during the final engineering stage. However, no runoff will be released from this project that will cause harm to lives or properties. Runoff will be released into the existing terrain through rip rap energy dissipaters at or below the erosive velocity (6 fps). Furthermore, on the steep sloping street, chevrons will be constructed at a interval that will reduce the quantity and the velocity of the runoff so that the runoff can be released safely into the natural ground.

DECLARATION OF RESPONSIBLE CHARGE

I hereby declare that I am the Engineer of Work for this project, that I have exercised responsible charge over the design of the project as defined in section 6703 of the business and professions code, and that the design is consistent with current standards.

| I understand that the check of project drawings and specifications by the County of Sa |
|--|
| Diego is confined to a review only and does not relieve me, as Engineer of Work, of m |
| responsibilities for project design. |

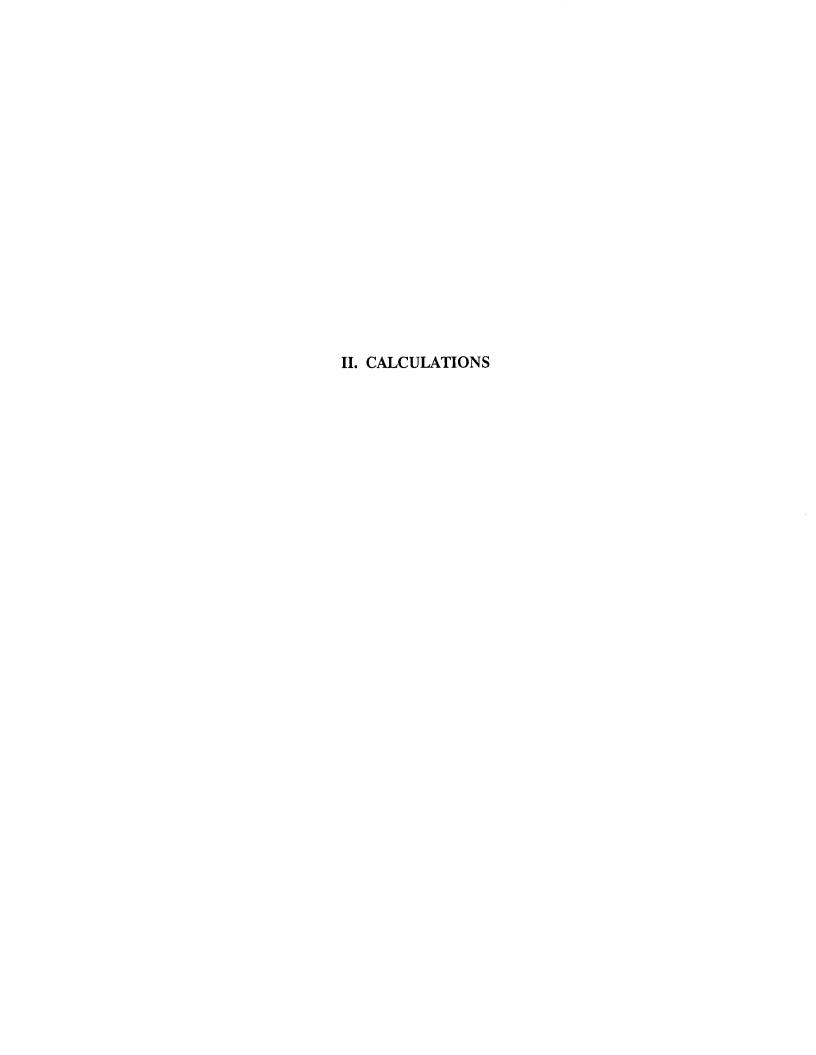
| Ronald L. Holloway | R.C.E. 29271 | Date | _ |
|--------------------|--------------|------|---|

DECLARATION OF RESPONSIBLE CHARGE

I hereby declare that I am the Engineer of Work for this project, that I have exercised responsible charge over the design of the project as defined in section 6703 of the business and professions code, and that the design is consistent with current standards.

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|---|
| Diego is confined to a review only and does not relieve me, as Engineer of Work, of my |
| responsibilities for project design. |

| Ronald L. Holloway | R.C.E. 29271 | Date |
|--------------------|--------------|------|



II. CALCULATIONS A. EXISTING HYDROLOGY

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT 2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2003 Advanced Engineering Software (aes) Ver. 1.5A Release Date: 01/01/2003 License ID 1459

Analysis prepared by:

bHA, Inc. 5115 Avenida Encinas, Suite L Carlsbad, Calif 92008

TIME/DATE OF STUDY: 13:05 04/04/2005 ______ USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: ______ 2003 SAN DIEGO MANUAL CRITERIA USER SPECIFIED STORM EVENT(YEAR) = 100.00 6-HOUR DURATION PRECIPITATION (INCHES) = SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00 SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR (FT) SIDE / SIDE / WAY (FT) (FT) (FT) (n) NO. (FT) 1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth) * (Velocity) Constraint = 6.0 (FT*FT/S) *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* HYDROLOGY FOR PIZZUTO PROPERTY | W.O. 555-0915-400 EXISTING BASIN 1 & 2 ************* FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21 _______ >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000 SOIL CLASSIFICATION IS "C"

```
S.C.S. CURVE NUMBER (AMC II) = 85
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 80.00
 UPSTREAM ELEVATION(FEET) = 1296.00
 DOWNSTREAM ELEVATION(FEET) = 1275.00
ELEVATION DIFFERENCE(FEET) = 21.00
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.979
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.217
 SUBAREA RUNOFF (CFS) = 0.27
                    0.11 TOTAL RUNOFF(CFS) =
 TOTAL AREA (ACRES) =
FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 51
______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <><<
________
 ELEVATION DATA: UPSTREAM(FEET) = 1275.00 DOWNSTREAM(FEET) = 860.00
 CHANNEL LENGTH THRU SUBAREA (FEET) = 1500.00 CHANNEL SLOPE = 0.2767
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00
  100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.525
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 85
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.76
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 9.73
 AVERAGE FLOW DEPTH(FEET) = 0.26 TRAVEL TIME(MIN.) = 2.57
 Tc(MIN.) = 8.55
                   13.60
                             SUBAREA RUNOFF(CFS) = 26.62
 SUBAREA AREA(ACRES) =
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
 TOTAL AREA(ACRES) = 13.71 PEAK FLOW RATE(CFS) = 26.84
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.38 FLOW VELOCITY(FEET/SEC.) = 12.31
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 3.00 = 1580.00 FEET.
 EXISTING 18" CSP PIPE
 UNDER CLAYTON PLACE
FLOW PROCESS FROM NODE 3.00 TO NODE 3.10 IS CODE = 41
______
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <<<<<
______
 ELEVATION DATA: UPSTREAM(FEET) = 860.00 DOWNSTREAM(FEET) = 850.00
 FLOW LENGTH (FEET) = 80.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.8 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 21.95
 GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 26.84
 PIPE TRAVEL TIME (MIN.) = 0.06 Tc (MIN.) = 8.61
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 3.10 = 1660.00 FEET.
```

```
FLOW PROCESS FROM NODE 3.10 TO NODE
                               14.00 \text{ IS CODE} = 51
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<
_______
 ELEVATION DATA: UPSTREAM(FEET) = 850.00 DOWNSTREAM(FEET) = 822.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 450.00 CHANNEL SLOPE = 0.0622 CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) =
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.056
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 85
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 28.31
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 7.61
 AVERAGE FLOW DEPTH(FEET) = 0.60 TRAVEL TIME(MIN.) =
         9.60
 Tc(MIN.) =
                          SUBAREA RUNOFF(CFS) = 2.94
 SUBAREA AREA(ACRES) = 1.62
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
 TOTAL AREA(ACRES) = 15.33 PEAK FLOW RATE(CFS) = 27.85
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.59 FLOW VELOCITY(FEET/SEC.) = 7.60
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 14.00 = 2110.00 FEET.
FLOW PROCESS FROM NODE
                 14.00 TO NODE 14.00 \text{ IS CODE} = 10
______
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
_______
****************
                               12.00 \text{ IS CODE} = 21
 FLOW PROCESS FROM NODE
                  11.00 TO NODE
______
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<
_______
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 85
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00
 UPSTREAM ELEVATION (FEET) = 1216.00
 DOWNSTREAM ELEVATION (FEET) = 1200.00
 ELEVATION DIFFERENCE (FEET) = 16.00
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.647
 SUBAREA RUNOFF (CFS) = 0.23
                 0.10 TOTAL RUNOFF(CFS) =
                                         0.23
 TOTAL AREA(ACRES) =
FLOW PROCESS FROM NODE 12.00 TO NODE 13.00 IS CODE = 51
 ______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<
______
```

```
CHANNEL LENGTH THRU SUBAREA(FEET) = 1210.00 CHANNEL SLOPE = 0.2893
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) =
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.510
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 85
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.54
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 10.65
 AVERAGE FLOW DEPTH(FEET) = 0.28 TRAVEL TIME(MIN.) = 1.89
 Tc(MIN.) = 8.58
                    16.60 SUBAREA RUNOFF(CFS) = 32.42
 SUBAREA AREA(ACRES) =
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
                                PEAK FLOW RATE(CFS) =
 TOTAL AREA(ACRES) = 16.70
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.42 FLOW VELOCITY(FEET/SEC.) = 13.42
                        11.00 TO NODE 13.00 = 1310.00 FEET.
 LONGEST FLOWPATH FROM NODE
FLOW PROCESS FROM NODE 13.00 TO NODE 14.00 IS CODE = 51
 ______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <>>>
ELEVATION DATA: UPSTREAM(FEET) = 850.00 DOWNSTREAM(FEET) = 822.00 CHANNEL LENGTH THRU SUBAREA(FEET) = 350.00 CHANNEL SLOPE = 0.0800
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.208
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 85
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 35.13
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 8.90
 AVERAGE FLOW DEPTH(FEET) = 0.63 TRAVEL TIME(MIN.) = 0.66
 Tc(MIN.) = 9.23
 SUBAREA AREA (ACRES) = 2.70 SUBAREA RUNOFF (CFS) = 5.03
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
                                 PEAK FLOW RATE(CFS) = 36.13
 TOTAL AREA (ACRES) = 19.40
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.64 FLOW VELOCITY(FEET/SEC.) = 8.93
                         11.00 TO NODE 14.00 = 1660.00 FEET.
 LONGEST FLOWPATH FROM NODE
************************
 FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 11
-----
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY << < >
** MAIN STREAM CONFLUENCE DATA **
 STREAM RUNOFF TC INTENSITY
                                     AREA
 NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

1 36.13 9.23 6.208 19.40

LONGEST FLOWPATH FROM NODE 11.00 TO NODE 14.00 = 1660.00 FEET.
```

ELEVATION DATA: UPSTREAM(FEET) = 1200.00 DOWNSTREAM(FEET) = 850.00

```
** MEMORY BANK # 1 CONFLUENCE DATA **
         RUNOFF TC INTENSITY
                                   AREA
 STREAM
 NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

1 27.85 9.60 6.056 15.33

LONGEST FLOWPATH FROM NODE 1.00 TO NODE 14.00 = 2110.00 FEET.
 ** PEAK FLOW RATE TABLE **

        STREAM
        RUNOFF
        Tc
        INTENSITY

        NUMBER
        (CFS)
        (MIN.)
        (INCH/HOUR)

        1
        62.94
        9.23
        6.208

        2
        63.10
        9.60
        6.056

 COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE (CFS) = 63.10
                             Tc(MIN.) = 9.60
 TOTAL AREA(ACRES) =
                    34.73
FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 12
 _____
 >>>>CLEAR MEMORY BANK # 1 <<<<<
_______
______
 END OF STUDY SUMMARY:
                                         9.60
                        34.73 \text{ TC}(MIN.) =
 TOTAL AREA (ACRES)
 PEAK FLOW RATE (CFS) = 63.10
```

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT 2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

bHA, Inc. 5115 Avenida Encinas, Suite L Carlsbad, Calif 92008

FILE NAME: K:\HYDRO\0915\EX3.DAT@@@@@@@@@@@@@@@@@@@@@@ TIME/DATE OF STUDY: 15:22 11/18/2004 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: 2003 SAN DIEGO MANUAL CRITERIA USER SPECIFIED STORM EVENT (YEAR) = 100.00 6-HOUR DURATION PRECIPITATION (INCHES) = SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00 SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR (FT) (FT) SIDE / SIDE / WAY (FT) (FT) (FT) (n) NO. ---- ----- -----===== === 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth) * (Velocity) Constraint = 6.0 (FT*FT/S) *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* +-----HYDROLOGY FOR PIZZUTO PROPERTY W.O. 555-0915-400 | EXISTING BASIN 3 ***************** FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 21

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000 SOIL CLASSIFICATION IS "C"

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<

```
S.C.S. CURVE NUMBER (AMC II) = 85
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 80.00
 UPSTREAM ELEVATION(FEET) = 1204.00
 DOWNSTREAM ELEVATION(FEET) = 1175.00
ELEVATION DIFFERENCE(FEET) = 29.00
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.979
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.217
 SUBAREA RUNOFF(CFS) = 0.67
 TOTAL AREA (ACRES) =
                    0.27 TOTAL RUNOFF (CFS) = 0.67
*********************
 FLOW PROCESS FROM NODE 22.00 TO NODE
                                   23.00 \text{ IS CODE} = 51
______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <>>>
ELEVATION DATA: UPSTREAM(FEET) = 1175.00 DOWNSTREAM(FEET) = 808.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1960.00 CHANNEL SLOPE = 0.1872
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) =
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.115
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 85
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.62
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 9.41
 AVERAGE FLOW DEPTH(FEET) = 0.33 TRAVEL TIME(MIN.) =
 Tc(MIN.) = 9.45
                   18.10
 SUBAREA AREA (ACRES) =
                            SUBAREA RUNOFF(CFS) = 33.21
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
 TOTAL AREA(ACRES) = 18.37 PEAK FLOW RATE(CFS) =
                                                  33.70
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.48 FLOW VELOCITY(FEET/SEC.) = 11.68
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 2040.00 FEET.
_______
 END OF STUDY SUMMARY:
 TOTAL AREA (ACRES) =
                      18.37 \text{ TC}(MIN.) =
 PEAK FLOW RATE (CFS) = 33.70
_______
```

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT 2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

bHA, Inc. 5115 Avenida Encinas, Suite L Carlsbad, Calif 92008

TIME/DATE OF STUDY: 15:29 11/18/2004 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: 2003 SAN DIEGO MANUAL CRITERIA USER SPECIFIED STORM EVENT (YEAR) = 100.00 6-HOUR DURATION PRECIPITATION (INCHES) = SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00 SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (n)NO. 1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S) *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* +----+ | HYDROLOGY FOR PIZZUTO PROPERTY W.O. 555-0915-400 | EXISTING BASIN 4 FLOW PROCESS FROM NODE 11.00 TO NODE 32.00 IS CODE = 21 ______

NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000 SOIL CLASSIFICATION IS "C"

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<

```
S.C.S. CURVE NUMBER (AMC II) = 85
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00
 UPSTREAM ELEVATION(FEET) = 1216.00
 DOWNSTREAM ELEVATION (FEET) = 1175.00
 ELEVATION DIFFERENCE (FEET) = 41.00
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.647
 SUBAREA RUNOFF (CFS) = 0.25
 TOTAL AREA (ACRES) =
                     0.11 TOTAL RUNOFF(CFS) = 0.25
********************
 FLOW PROCESS FROM NODE 32.00 TO NODE
                                   33.00 \text{ IS CODE} = 51
 _____
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<
_______
 ELEVATION DATA: UPSTREAM(FEET) = 1175.00 DOWNSTREAM(FEET) = 985.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 650.00 CHANNEL SLOPE = 0.2923 CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) =
  100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.571
 NATURAL DESERT LANDSCAPING RUNOFF COEFFICIENT = .3000
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 85
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.76
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 6.12
                                               1.77
 AVERAGE FLOW DEPTH(FEET) = 0.12 TRAVEL TIME(MIN.) =
 Tc(MIN.) = 8.46
 SUBAREA AREA (ACRES) = 3.53 SUBAREA RUNOFF (CFS) = 6.96
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
 TOTAL AREA(ACRES) = 3.64 PEAK FLOW RATE(CFS) = 7.18
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.17 FLOW VELOCITY(FEET/SEC.) = 7.87
 LONGEST FLOWPATH FROM NODE 11.00 TO NODE 33.00 = 750.00 FEET.
______
 END OF STUDY SUMMARY:
 TOTAL AREA (ACRES) = 3.64 TC (MIN.) = PEAK FLOW RATE (CFS) = 7.18
_______
```

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT 2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

bHA, Inc. 5115 Avenida Encinas, Suite L Carlsbad, Calif 92008

TIME/DATE OF STUDY: 08:32 12/06/2004 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: 2003 SAN DIEGO MANUAL CRITERIA USER SPECIFIED STORM EVENT (YEAR) = 100.00 6-HOUR DURATION PRECIPITATION (INCHES) = 3.500 SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00 SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR (FT) (FT) SIDE / SIDE / WAY (FT) (FT) (FT) (n) NO. ---- ----- -----1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S) *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* +-----| HYDROLOGY FOR PIZZUTO PROPERTY W.O. 555-0915-400 | EXISTING BASIN 5 ***************** FLOW PROCESS FROM NODE 40.00 TO NODE 41.00 IS CODE = 21 ______ >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS

RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600 SOIL CLASSIFICATION IS "C"

```
S.C.S. CURVE NUMBER (AMC II) = 76
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 90.00
 UPSTREAM ELEVATION (FEET) = 962.50
 DOWNSTREAM ELEVATION(FEET) = 900.00
ELEVATION DIFFERENCE(FEET) = 62.50
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.866
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 8.319
 SUBAREA RUNOFF(CFS) = 0.18
                    0.06 TOTAL RUNOFF(CFS) =
 TOTAL AREA (ACRES) =
41.00 TO NODE
                                  42.00 \text{ IS CODE} = 51
 FLOW PROCESS FROM NODE
 ______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<
________
 ELEVATION DATA: UPSTREAM(FEET) = 900.00 DOWNSTREAM(FEET) = 868.00 CHANNEL LENGTH THRU SUBAREA(FEET) = 380.00 CHANNEL SLOPE = 0.0842 CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH (FEET) = 1.00
 CHANNEL FLOW THRU SUBAREA(CFS) = 0.18
FLOW VELOCITY(FEET/SEC.) = 1.29 FLOW DEPTH(FEET) = 0.03
TRAVEL TIME(MIN.) = 4.93 Tc(MIN.) = 10.79
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE
                                       42.00 = 470.00 FEET.
    ______
| BROW DITCH IS ANALYSIS AS IF
| IT WAS A 36" PIPE FLOWING NO MORE THAN
| HALF FULL
FLOW PROCESS FROM NODE 42.00 TO NODE 43.00 IS CODE = 41
                     ______
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <><<
_______
 ELEVATION DATA: UPSTREAM(FEET) = 868.00 DOWNSTREAM(FEET) = 805.00
 FLOW LENGTH (FEET) = 760.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 0.9 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 4.12
 GIVEN PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES =
 PIPE-FLOW(CFS) = 0.18
 PIPE TRAVEL TIME (MIN.) = 3.08 Tc (MIN.) = 13.87
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 43.00 = 1230.00 FEET.
*****************
 FLOW PROCESS FROM NODE 42.00 TO NODE 43.00 IS CODE = 81
_____
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<
_______
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.775
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600
```

SUBAREA AREA (ACRES) = 4.18 SUBAREA RUNOFF (CFS) = 7.19

TOTAL AREA (ACRES) = 4.24 TOTAL RUNOFF (CFS) = 7.29

TC (MIN.) = 13.87

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 4.24 TC (MIN.) = 13.87

PEAK FLOW RATE (CFS) = 7.29

II. CALCULATIONS B. PROPOSED HYDROLOGY

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT 2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

BHA, INC 5115 Avenida Encinas Suite L Carlsbad, CA 92008 (760) 931-8700

FILE NAME: K:\HYDRO\0915\P1.DAT TIME/DATE OF STUDY: 01:22 09/08/2006 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: ______ 2003 SAN DIEGO MANUAL CRITERIA USER SPECIFIED STORM EVENT (YEAR) = 100.00 6-HOUR DURATION PRECIPITATION (INCHES) = SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00 SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (n) NO. 1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth) * (Velocity) Constraint = 6.0 (FT*FT/S)*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* +----+ | HYDROLOGY FOR PIZZUTO PROPERTY | W.O. 555-0915-400 PROPOSED BASIN 1 & 2 ****************** FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21 _____ >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600 SOIL CLASSIFICATION IS "C" S.C.S. CURVE NUMBER (AMC II) = 76 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00 UPSTREAM ELEVATION (FEET) = 1296.00

DOWNSTREAM ELEVATION (FEET) = 1275.00

```
ELEVATION DIFFERENCE (FEET) = 21.00
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.530
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN To CALCULATION!
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 8.641
 SUBAREA RUNOFF (CFS) = 0.34
 TOTAL AREA(ACRES) =
                   0.11 TOTAL RUNOFF (CFS) = 0.34
**************
 FLOW PROCESS FROM NODE
                    2.00 TO NODE
                                3.00 \text{ IS CODE} = 51
______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <
______
 ELEVATION DATA: UPSTREAM(FEET) = 1275.00 DOWNSTREAM(FEET) = 860.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1500.00 CHANNEL SLOPE = 0.2767
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.876
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.40
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 10.64
 AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 2.35
 Tc(MIN.) = 7.88
 SUBAREA AREA(ACRES) = 13.60 SUBAREA RUNOFF(CFS) = 33.67
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.360
 TOTAL AREA(ACRES) = 13.71 PEAK FLOW RATE(CFS) = 33.94
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.43 FLOW VELOCITY(FEET/SEC.) = 13.40
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 3.00 = 1580.00 FEET.
***************
 FLOW PROCESS FROM NODE 3.00 TO NODE 3.10 IS CODE = 41
______
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <>>>
______
 ELEVATION DATA: UPSTREAM(FEET) = 860.00 DOWNSTREAM(FEET) = 850.00
 FLOW LENGTH (FEET) = 80.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 11.2 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 23.48
 GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 33.94
 PIPE TRAVEL TIME (MIN.) = 0.06
                          Tc(MIN.) = 7.94
                        1.00 TO NODE 3.10 = 1660.00 FEET.
 LONGEST FLOWPATH FROM NODE
*****************
 FLOW PROCESS FROM NODE 3.10 TO NODE 14.00 IS CODE = 51
 ______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <>>>
ELEVATION DATA: UPSTREAM(FEET) = 850.00 DOWNSTREAM(FEET) = 822.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 450.00 CHANNEL SLOPE = 0.0622
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.390
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
```

```
S.C.S. CURVE NUMBER (AMC II) = 76
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 38.54
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 8.39
 AVERAGE FLOW DEPTH(FEET) = 0.71 TRAVEL TIME(MIN.) = 0.89
 Tc(MIN.) = 8.83
 SUBAREA AREA (ACRES) = 4.00 SUBAREA RUNOFF (CFS) = 9.20
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.360
 TOTAL AREA(ACRES) = 17.71 PEAK FLOW RATE(CFS) = 40.74
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.74 FLOW VELOCITY(FEET/SEC.) = 8.54
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 14.00 = 2110.00 FEET.
*******************
 FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 10
_____
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
_______
***************
 FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 21
______
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<
_______
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00
 UPSTREAM ELEVATION(FEET) = 1175.00
 DOWNSTREAM ELEVATION(FEET) = 1174.00
ELEVATION DIFFERENCE(FEET) = 1.00
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 11.144
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
        THE MAXIMUM OVERLAND FLOW LENGTH = 70.00
        (Reference: Table 3-1B of Hydrology Manual)
        THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.499
 SUBAREA RUNOFF (CFS) = 0.20
                   0.10 TOTAL RUNOFF(CFS) = 0.20
 TOTAL AREA(ACRES) =
*************
 FLOW PROCESS FROM NODE 12.00 TO NODE 12.10 IS CODE = 51
______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <>
______
 ELEVATION DATA: UPSTREAM(FEET) = 1174.00 DOWNSTREAM(FEET) = 1072.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 250.00 CHANNEL SLOPE = 0.4080
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.296
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.24
 AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 0.67
 Tc(MIN.) = 11.81
 SUBAREA AREA (ACRES) = 2.80 SUBAREA RUNOFF (CFS) = 5.34
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.360
 TOTAL AREA(ACRES) = 2.90 PEAK FLOW RATE(CFS) = 5.53
```

```
END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.13 FLOW VELOCITY(FEET/SEC.) = 7.92
 LONGEST FLOWPATH FROM NODE 11.00 TO NODE 12.10 = 350.00 FEET.
****************
                   12.10 TO NODE 12.20 IS CODE = 41
 FLOW PROCESS FROM NODE
______
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <<<<
ELEVATION DATA: UPSTREAM(FEET) = 1072.00 DOWNSTREAM(FEET) = 1066.00
 FLOW LENGTH (FEET) = 45.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.7 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 14.87
 GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) =
               5.53
 PIPE TRAVEL TIME (MIN.) = 0.05 Tc (MIN.) = 11.86
 LONGEST FLOWPATH FROM NODE 11.00 TO NODE 12.20 = 395.00 FEET.
| BEGIN BROW DITCH ANALYSIS
| BROW DITCH ANALYSIS AS IF IT WAS A 36 INCH
| PIPE FLOWING NO MORE THAN HALF FULL.
 · -----
*******************
 FLOW PROCESS FROM NODE 12.20 TO NODE 12.30 IS CODE = 41
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <<<<
ELEVATION DATA: UPSTREAM(FEET) = 1066.00 DOWNSTREAM(FEET) = 980.00
 FLOW LENGTH (FEET) = 425.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 3.5 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 15.81
 GIVEN PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 5.53
 PIPE TRAVEL TIME (MIN.) = 0.45 Tc (MIN.) = 12.31
 LONGEST FLOWPATH FROM NODE 11.00 TO NODE 12.30 = 820.00 FEET.
******************
 FLOW PROCESS FROM NODE 12.20 TO NODE 12.30 IS CODE = 81
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.157
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600
 SUBAREA AREA(ACRES) = 5.20 SUBAREA RUNOFF(CFS) = 9.65
TOTAL AREA(ACRES) = 8.10 TOTAL RUNOFF(CFS) = 15.04
 TC(MIN.) = 12.31
*******************
                              12.40 \text{ IS CODE} = 41
 FLOW PROCESS FROM NODE 12.30 TO NODE
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <<<<
```

```
ELEVATION DATA: UPSTREAM(FEET) = 980.00 DOWNSTREAM(FEET) = 955.00
 FLOW LENGTH (FEET) = 85.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 26.19
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 15.04
 PIPE TRAVEL TIME (MIN.) = 0.05 Tc (MIN.) = 12.36
 LONGEST FLOWPATH FROM NODE 11.00 TO NODE 12.40 =
 BEGIN BROW DITCH
*****************
 FLOW PROCESS FROM NODE 12.40 TO NODE 12.50 IS CODE = 41
 _____
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <><<
______
 ELEVATION DATA: UPSTREAM(FEET) = 955.00 DOWNSTREAM(FEET) = 880.00
 FLOW LENGTH (FEET) = 170.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 4.7 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 28.04
 GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 15.04
 PIPE TRAVEL TIME (MIN.) = 0.10 Tc (MIN.) = 12.47
 LONGEST FLOWPATH FROM NODE
                     11.00 TO NODE 12.50 = 1075.00 FEET.
***************
 FLOW PROCESS FROM NODE 12.50 TO NODE 12.50 IS CODE = 10
 _____
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<
**************
 FLOW PROCESS FROM NODE 13.00 TO NODE 13.10 IS CODE = 21
 _____
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<
RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 INITIAL SUBAREA FLOW-LENGTH (FEET) =
 UPSTREAM ELEVATION(FEET) = 1150.00
 DOWNSTREAM ELEVATION(FEET) = 13.10
ELEVATION DIFFERENCE(FEET) = 1136.90
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.183
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN To CALCULATION!
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 8.041
 SUBAREA RUNOFF (CFS) = 0.72
                  0.25 TOTAL RUNOFF(CFS) =
 TOTAL AREA(ACRES) =
******************
 FLOW PROCESS FROM NODE 13.10 TO NODE 12.50 IS CODE = 41
_____
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <>>>
______
 ELEVATION DATA: UPSTREAM(FEET) = 1130.00 DOWNSTREAM(FEET) = 880.00
```

```
FLOW LENGTH (FEET) = 600.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 1.1 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 10.97
 GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 0.72
 PIPE TRAVEL TIME (MIN.) = 0.91 Tc (MIN.) = 7.09
 LONGEST FLOWPATH FROM NODE 13.00 TO NODE 12.50 = 700.00 FEET.
****************
 FLOW PROCESS FROM NODE 13.10 TO NODE 12.50 IS CODE = 81
 ______
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.358
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3600
 SUBAREA AREA(ACRES) = 4.90 SUBAREA RUNOFF(CFS) = 12.98
TOTAL AREA(ACRES) = 5.15 TOTAL RUNOFF(CFS) = 13.64
 TOTAL AREA(ACRES) =
 TC(MIN.) = 7.09
*****************
 FLOW PROCESS FROM NODE 12.50 TO NODE 12.50 IS CODE = 11
 ______
 >>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<
______
 ** MAIN STREAM CONFLUENCE DATA **
 STREAM RUNOFF TC INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

1 13.64 7.09 7.358 5.15
LONGEST FLOWPATH FROM NODE 13.00 TO NODE 12.50 = 700.00 FEET.
 ** MEMORY BANK # 2 CONFLUENCE DATA **

STREAM RUNOFF TC INTENSITY AREA

NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

1 15.04 12.47 5.116 8.10

LONGEST FLOWPATH FROM NODE 11.00 TO NODE 12.50 = 1075.00 FEET.
 ** PEAK FLOW RATE TABLE **
 STREAM RUNOFF TC INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 22.20 7.09 7.358
2 24.52 12.47 5.116
 COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE (CFS) = 24.52 Tc (MIN.) = 12.47
 TOTAL AREA(ACRES) =
*************
 FLOW PROCESS FROM NODE 12.50 TO NODE 12.50 IS CODE = 12
______
 >>>>CLEAR MEMORY BANK # 2 <<<<
**************
 FLOW PROCESS FROM NODE 12.50 TO NODE 12.60 IS CODE = 41
______
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <><<
```

```
ELEVATION DATA: UPSTREAM(FEET) = 880.00 DOWNSTREAM(FEET) = 864.00
 FLOW LENGTH (FEET) = 135.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 9.5 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 21.13
 GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 24.52
 PIPE TRAVEL TIME (MIN.) = 0.11 Tc (MIN.) = 12.57
 LONGEST FLOWPATH FROM NODE
                        11.00 TO NODE 12.60 = 1210.00 FEET.
******************
 FLOW PROCESS FROM NODE 12.60 TO NODE 14.00 IS CODE = 51
______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<
______
 ELEVATION DATA: UPSTREAM(FEET) = 864.00 DOWNSTREAM(FEET) = 822.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 400.00 CHANNEL SLOPE = 0.1050 CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00
  100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.907
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 30.07
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.22
 AVERAGE FLOW DEPTH(FEET) = 0.54 TRAVEL TIME(MIN.) = 0.72
 Tc(MIN.) = 13.30
 SUBAREA AREA(ACRES) = 6.28 SUBAREA RUNOFF(CFS) = 11.09
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.360
 TOTAL AREA(ACRES) = 19.53
                              PEAK FLOW RATE(CFS) =
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.58 FLOW VELOCITY(FEET/SEC.) = 9.72
 LONGEST FLOWPATH FROM NODE 11.00 TO NODE 14.00 = 1610.00 FEET.
*****************
 FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 11
 _____
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<
** MAIN STREAM CONFLUENCE DATA **
 STREAM RUNOFF TC INTENSITY AREA
       (CFS)
 NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 34.50 13.30 4.907 19.53
LONGEST FLOWPATH FROM NODE 11.00 TO NODE 14.00 = 1610.00 FEET.
 ** MEMORY BANK # 1 CONFLUENCE DATA **
 STREAM RUNOFF TC INTENSITY
                                    AREA
 NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 40.74 8.83 6.390 17.71
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 14.00 = 2110.00 FEET.
 ** PEAK FLOW RATE TABLE **
 STREAM RUNOFF To INTENSITY
 NUMBER
         (CFS)
                  (MIN.) (INCH/HOUR)
          63.65
                  8.83 6.390
    1
                              4.907
         65.79
                  13.30
```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 65.79 TOTAL AREA(ACRES) = 37.24 Tc(MIN.) = 13.30******************** 14.00 IS CODE = 1214.00 TO NODE FLOW PROCESS FROM NODE >>>>CLEAR MEMORY BANK # 1 <<<< ______ END OF STUDY SUMMARY: TOTAL AREA(ACRES) 37.24 TC (MIN.) = 13.30 PEAK FLOW RATE(CFS) = 65.79 _______ _______

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT 2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

bHA, Inc. 5115 Avenida Encinas, Suite L Carlsbad, Calif 92008

TIME/DATE OF STUDY: 14:14 12/01/2004 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: ._____ 2003 SAN DIEGO MANUAL CRITERIA USER SPECIFIED STORM EVENT (YEAR) = 100.00 6-HOUR DURATION PRECIPITATION (INCHES) = SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00 SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (T) 1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth) * (Velocity) Constraint = 6.0 (FT*FT/S) *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* +----+ HYDROLOGY FOR PIZZUTO PROPERTY W.O. 555-0915-400 PROPOSED BASIN 3 ******************* FLOW PROCESS FROM NODE 17.00 TO NODE 22.00 IS CODE = 21 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS< _______ RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600

SOIL CLASSIFICATION IS "C"

```
S.C.S. CURVE NUMBER (AMC II) = 76
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00
 UPSTREAM ELEVATION(FEET) = 1185.00
 DOWNSTREAM ELEVATION(FEET) = 1183.00
ELEVATION DIFFERENCE(FEET) = 2.00
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 9.747
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
        THE MAXIMUM OVERLAND FLOW LENGTH = 85.00
        (Reference: Table 3-1B of Hydrology Manual)
        THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.995
 SUBAREA RUNOFF(CFS) = 0.65
                    0.30
                         TOTAL RUNOFF(CFS) =
 TOTAL AREA (ACRES) =
FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 51
_____
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <>>>
________
 ELEVATION DATA: UPSTREAM(FEET) = 1183.00 DOWNSTREAM(FEET) = 808.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1940.00 CHANNEL SLOPE = 0.1933
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00
  100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.934
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.84
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.41
 AVERAGE FLOW DEPTH(FEET) = 0.32 TRAVEL TIME(MIN.) = 3.44
 Tc(MIN.) = 13.18
 SUBAREA AREA(ACRES) = 18.07 SUBAREA RUNOFF(CFS) = 32.10
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.360
                              PEAK FLOW RATE (CFS) = 32.63
 TOTAL AREA (ACRES) = 18.37
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.47 FLOW VELOCITY(FEET/SEC.) = 11.68
 LONGEST FLOWPATH FROM NODE 17.00 TO NODE 23.00 = 2040.00 FEET.
______
 END OF STUDY SUMMARY:
 TOTAL AREA(ACRES) = 18.37 TC(MIN.) = PEAK FLOW RATE(CFS) = 32.63
______
```

* ********************

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT 2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

bHA, Inc. 5115 Avenida Encinas, Suite L Carlsbad, Calif 92008

TIME/DATE OF STUDY: 14:19 12/01/2004 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: ._____ 2003 SAN DIEGO MANUAL CRITERIA USER SPECIFIED STORM EVENT (YEAR) = 100.00 6-HOUR DURATION PRECIPITATION (INCHES) = SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00 SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (n) NO. ____ ==== ======= 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S) *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* | HYDROLOGY FOR PIZZUTO PROPERTY W.O. 555-0915-400 PROPOSED BASIN 4 FLOW PROCESS FROM NODE 31.00 TO NODE 32.00 IS CODE = 21

RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600 SOIL CLASSIFICATION IS "C"

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS

```
S.C.S. CURVE NUMBER (AMC II) = 76
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00
 UPSTREAM ELEVATION (FEET) = 1175.00
 DOWNSTREAM ELEVATION (FEET) = 1173.00
 ELEVATION DIFFERENCE (FEET) =
 SUBAREA OVERLAND TIME OF FLOW(MIN.) =
                                9.747
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
        THE MAXIMUM OVERLAND FLOW LENGTH = 85.00
        (Reference: Table 3-1B of Hydrology Manual)
        THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.995
 SUBAREA RUNOFF(CFS) = 0.65
 TOTAL AREA(ACRES) =
                   0.30
                          TOTAL RUNOFF(CFS) =
FLOW PROCESS FROM NODE 32.00 TO NODE 33.00 IS CODE = 51
 ______
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<
ELEVATION DATA: UPSTREAM(FEET) = 1173.00 DOWNSTREAM(FEET) = 985.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 650.00 CHANNEL SLOPE = 0.2892
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) =
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.395
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 6.25
 AVERAGE FLOW DEPTH(FEET) = 0.12 TRAVEL TIME(MIN.) =
 Tc(MIN.) = 11.48
 SUBAREA AREA(ACRES) = 3.34 SUBAREA RUNOFF(CFS) = 6.49
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.360
 TOTAL AREA(ACRES) = 3.64
                              PEAK FLOW RATE (CFS) = 7.07
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:
 DEPTH(FEET) = 0.17 FLOW VELOCITY(FEET/SEC.) = 7.75
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 33.00 = 750.00 FEET.
_______
 END OF STUDY SUMMARY:
 TOTAL AREA(ACRES) = 3.64 TC(MIN.) = PEAK FLOW RATE(CFS) = 7.07
______
______
```

END OF RATIONAL METHOD ANALYSIS



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT 2003,1985,1981 HYDROLOGY MANUAL

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Analysis prepared by:

bHA, Inc. 5115 Avenida Encinas, Suite L Carlsbad, Calif 92008

FILE NAME: K:\HYDRO\0915\P5.DATSTGGGGGGGGGGGGGGGGGGGGGGGGGGGGG TIME/DATE OF STUDY: 08:39 12/06/2004 USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION: 2003 SAN DIEGO MANUAL CRITERIA USER SPECIFIED STORM EVENT(YEAR) = 100.00 6-HOUR DURATION PRECIPITATION (INCHES) = SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90 SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL* HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (n) 1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150 GLOBAL STREET FLOW-DEPTH CONSTRAINTS: 1. Relative Flow-Depth = 0.00 FEET as (Maximum Allowable Street Flow Depth) - (Top-of-Curb) 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S) *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.* HYDROLOGY FOR PIZZUTO PROPERTY W.O. 555-0915-400 | PROPOSED BASIN 5 ************************* FLOW PROCESS FROM NODE 40.00 TO NODE 41.00 IS CODE = 21 ______ >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<

RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600

SOIL CLASSIFICATION IS "C"

```
S.C.S. CURVE NUMBER (AMC II) = 76
  INITIAL SUBAREA FLOW-LENGTH (FEET) = 90.00
  UPSTREAM ELEVATION(FEET) = 962.50
  DOWNSTREAM ELEVATION(FEET) = 900.00
ELEVATION DIFFERENCE(FEET) = 62.50
  SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.866
  WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN To CALCULATION!
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.319
  SUBAREA RUNOFF (CFS) = 0.18
  TOTAL AREA(ACRES) =
                      0.06 TOTAL RUNOFF(CFS) = 0.18
***********************************
  FLOW PROCESS FROM NODE 41.00 TO NODE
                                     42.00 \text{ IS CODE} = 51
 >>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<<
ELEVATION DATA: UPSTREAM(FEET) = 900.00 DOWNSTREAM(FEET) = 868.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 380.00 CHANNEL SLOPE = 0.0842
 CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 2.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00
 CHANNEL FLOW THRU SUBAREA(CFS) = 0.18
FLOW VELOCITY(FEET/SEC.) = 1.29 FLOW DEPTH(FEET) = 0.03
TRAVEL TIME(MIN.) = 4.93 Tc(MIN.) = 10.79
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE
                                           42.00 = 470.00 \text{ FEET}.
********************************
 FLOW PROCESS FROM NODE 42.00 TO NODE 43.00 IS CODE = 61
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<
 >>>> (STANDARD CURB SECTION USED) <<<<
UPSTREAM ELEVATION(FEET) = 868.00 DOWNSTREAM ELEVATION(FEET) = 805.00
 STREET LENGTH(FEET) = 418.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH (FEET) = 14.00
 DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 9.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020
 SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) =
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200
   **TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =
   STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
   STREET FLOW DEPTH(FEET) = 0.26
   HALFSTREET FLOOD WIDTH (FEET) = 6.79
   AVERAGE FLOW VELOCITY (FEET/SEC.) = 7.24
   PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.90
 STREET FLOW TRAVEL TIME (MIN.) = 0.96 Tc (MIN.) = 11.76
  100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.313
 RESIDENTIAL (1. DU/AC OR LESS) RUNOFF COEFFICIENT = .3600
 SOIL CLASSIFICATION IS "C"
 S.C.S. CURVE NUMBER (AMC II) = 76
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.360
```

SUBAREA AREA (ACRES) = 4.18 SUBAREA RUNOFF (CFS) = 7.99
TOTAL AREA (ACRES) = 4.24 PEAK FLOW RATE (CFS) = 8.11

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH (FEET) = 0.31 HALFSTREET FLOOD WIDTH (FEET) = 9.25
FLOW VELOCITY (FEET/SEC.) = 8.32 DEPTH*VELOCITY (FT*FT/SEC.) = 2.59
LONGEST FLOWPATH FROM NODE 40.00 TO NODE 43.00 = 888.00 FEET.

END OF STUDY SUMMARY:
TOTAL AREA (ACRES) = 4.24 TC (MIN.) = 11.76
PEAK FLOW RATE (CFS) = 8.11

END OF RATIONAL METHOD ANALYSIS

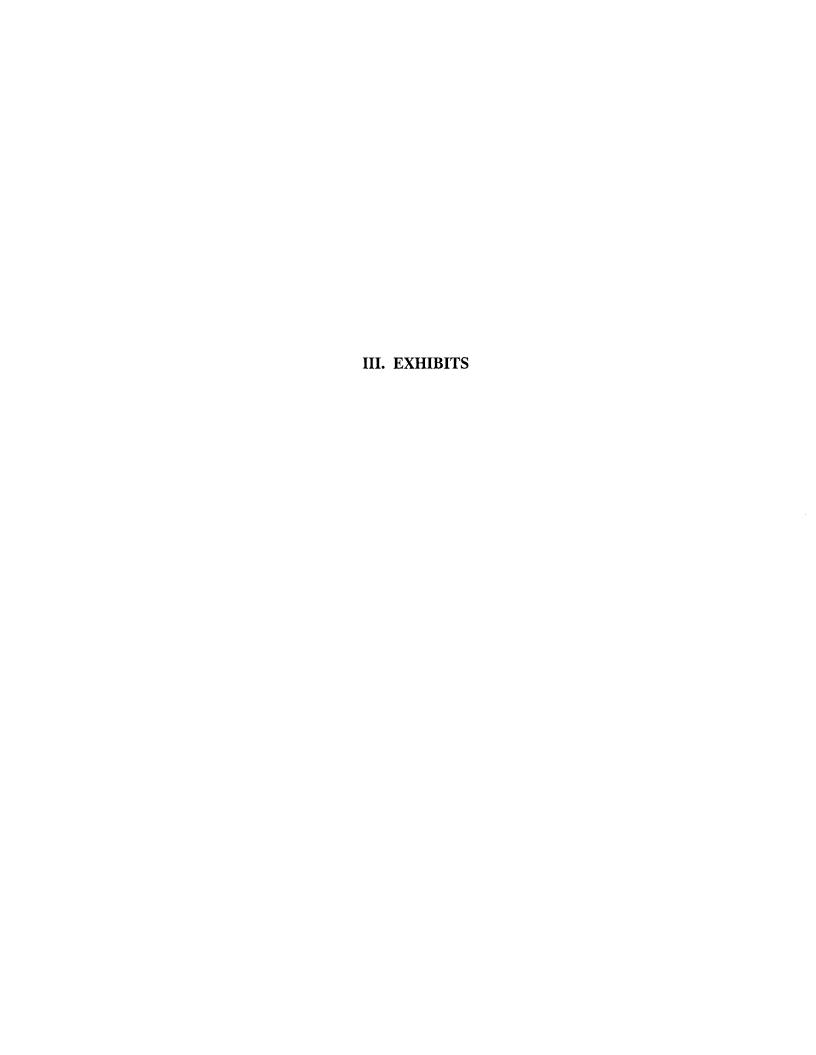
II. CALCULATIONSC. PROPOSED HYDRAULIC

tmp#2.txt

Manning Pipe Calculator

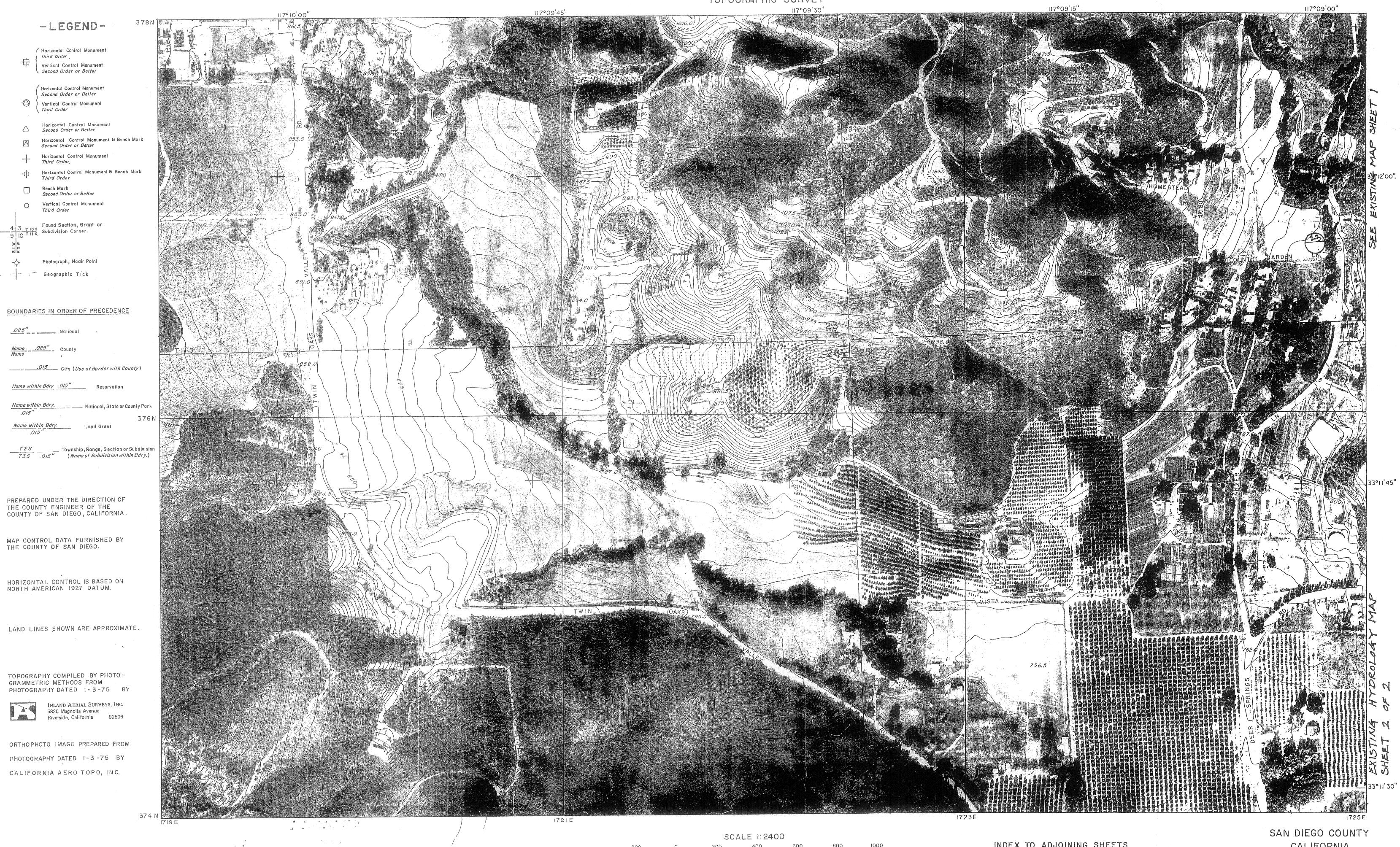
24-Inch Pipe at Node 3.0

| - | |
|--|--|
| Given Input Data: Shape Solving for Diameter Flowrate Slope Manning's n | Circular Depth of Flow 2.0000 ft 40.5000 cfs 0.1250 ft/ft 0.0135 |
| Computed Results: Depth Area Wetted Area Wetted Perimeter Perimeter Velocity Hydraulic Radius Percent Full Full flow Flowrate Full flow velocity | 1.0303 ft 3.1416 ft2 1.6314 ft2 3.2023 ft 6.2832 ft 24.8247 fps 0.5095 ft 51.5164 % 77.0200 cfs 24.5162 fps |



COUNTY OF SAN DIEGO

TOPOGRAPHIC SURVEY



PRECISION OCT 15 1975 MICROFILMED CONTOUR INTERVAL 5 FEET

U.S.C. & G.S. SEA LEVEL DATUM OF 1929 TWO THOUSAND FOOT CALIFORNIA RECTANGULAR GRID (ZONE VI) THE LAST THREE DIGITS OF THE GRID NUMBERS ARE OMITTED THE RECTANGULAR COORDINATE VALUES ARE SHOWN ON THE SOUTH AND WEST MARGINS
THE GEOGRAPHIC VALUES ARE SHOWN ON THE NORTH AND EAST MARGINS

INDEX TO ADJOINING SHEETS

378-1713 378-1719 378-1725 374-1713 374-1719 374-1725 370-1713 370-1719 370-1725 PIZZUTO PROPERTY

CALIFORNIA

EDITION OF 1975

SHEET 374-1719

COUNTY OF SAN DIEGO TOPOGRAPHIC SURVEY 117°08'45" 117°08'15" 117°08'00" LEGEND-Horizontal Control Monument Third Order Vertical Control Manument Second Order or Better / Horizontal Control Monument Second Order or Better Vertical Control Monument Horizontal Control Monument Second Order or Better Horizontal Control Monument & Bench Mark Second Order or Better Horizontal Control Monument Horizontal Control Manument & Bench Mark Third Order Bench Mork Second Order or Better Vertical Control Monument Third Order . Found Section, Grant or Photograph, Nadir Paint Geographic Tick BOUNDARIES IN ORDER OF PRECEDENCE .025" National Nome .025" County Name within Bdry 015" Reservation Name within Bdry, National, State or County Park Name within Bdry. __ Township, Ronge, Section or Subdivision (Name of Subdivision within Bdry.) PREPARED UNDER THE DIRECTION OF THE COUNTY ENGINEER OF THE COUNTY OF SAN DIEGO, CALIFORNIA. MAP CONTROL DATA FURNISHED BY THE COUNTY OF SAN DIEGO. HORIZONTAL CONTROL IS BASED ON NORTH AMERICAN 1927 DATUM. SPRINGS 806.0 LAND LINES SHOWN ARE APPROXIMATE. TOPOGRAPHY COMPILED BY PHOTO-GRAMMETRIC METHODS FROM PHOTOGRAPHY DATED 1-3-75 BY INLAND AERIAL SURVEYS, INC. 5826 Magnolia Avenue Riverside, California 92506 ORTHOPHOTO IMAGE PREPARED FROM PHOTOGRAPHY DATED 1-3-75 BY CALIFORNIA AERO TOPO, INC. 1727E 1729E LEGEND SCALE 1:2400 SAN DIEGO COUNTY NODE INDEX TO ADJOINING SHEETS CALIFORNIA Q (Cfs)
 378 - 1719
 378 - 1725
 378 - 1731

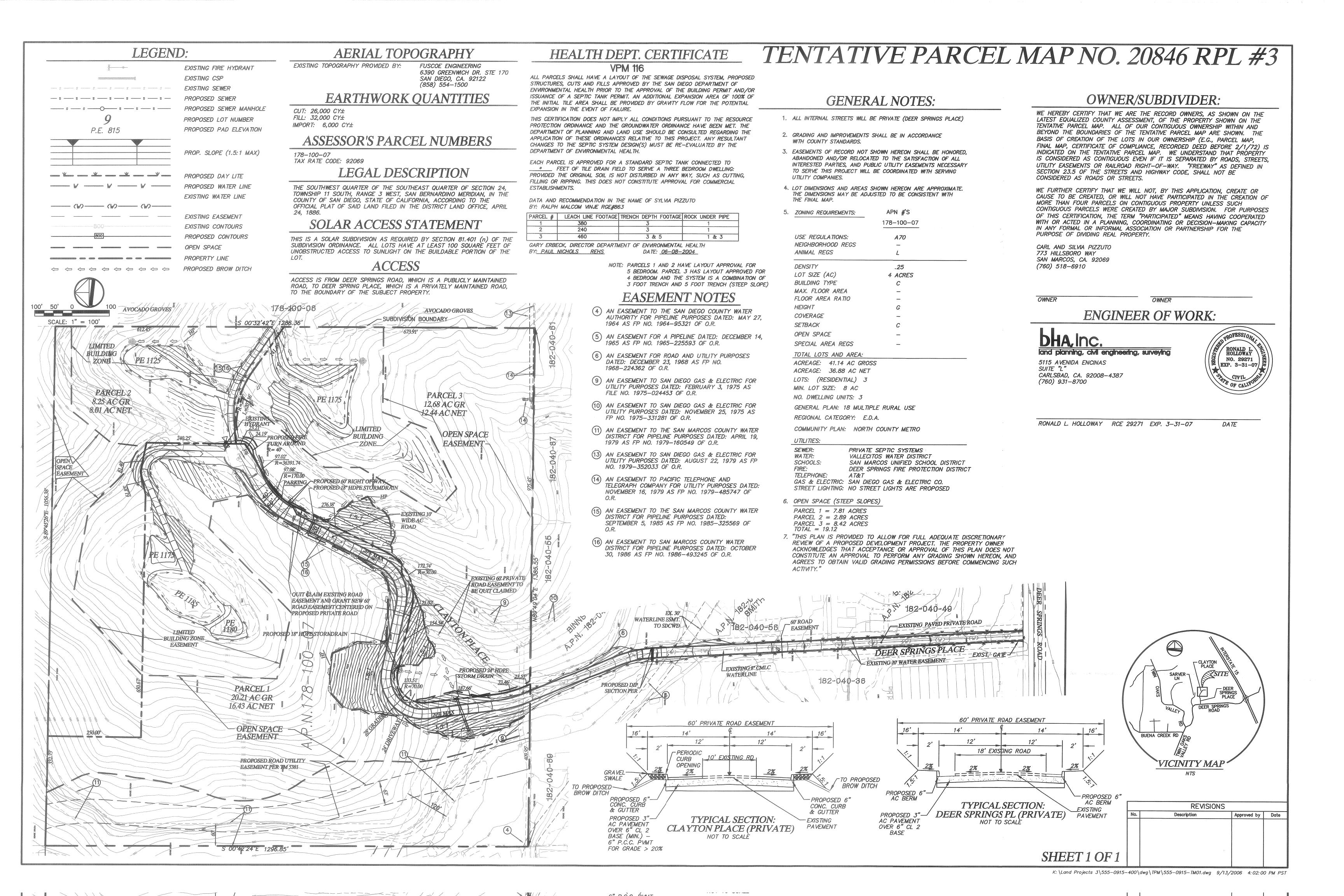
 374 - 1719
 374 - 1725
 374 - 1731

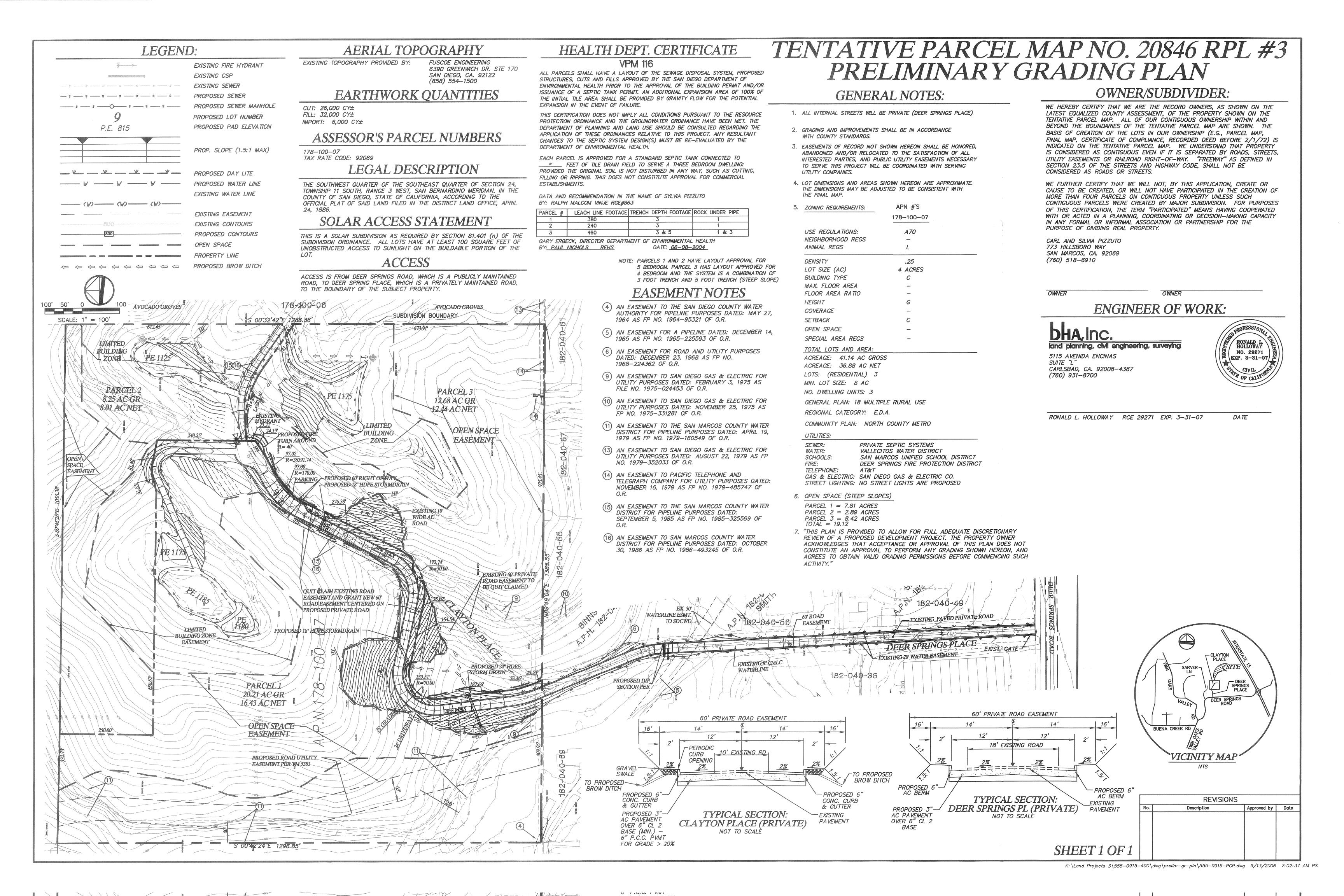
 370 - 1719
 370 - 1725
 370 - 1731
 CONTOUR INTERVAL 5 FEET Precision AREA (ACRE) EDITION OF 1975 U.S.C. & G.S. SEA LEVEL DATUM OF 1929 OCT 15 1975 BASIN # TWO THOUSAND FOOT CALIFORNIA RECTANGULAR GRID (ZONE VI) MICROFILMED PIZZUTO PROPERTY THE LAST THREE DIGITS OF THE GRID NUMBERS ARE OMITTED

THE RECTANGULAR COORDINATE VALUES ARE SHOWN ON THE SOUTH AND WEST MARGINS THE GEOGRAPHIC VALUES ARE SHOWN ON THE NORTH AND EAST MARGINS

FLOW PATH

SHEET 374-1725







8

AN E

Directions for Application:

- (1) From precipitation maps determine 6 hr and 24 hr amounts for the selected frequency. These maps are included in the County Hydrology Manual (10, 50, and 100 yr maps included in the Design and Procedure Manual).
 - (2) Adjust 6 hr precipitation (if necessary) so that it is within the range of 45% to 65% of the 24 hr precipitation (not applicable to Desert).
- (3) Plot 6 hr precipitation on the right side of the chart.
- (4) Draw a line through the point parallel to the plotted lines.
 - (5) This line is the intensity-duration curve for the location being analyzed.

Application Form:

- (a) Selected frequency /oo year
- (b) $P_6 = 3.5$ in., $P_{24} = 6.7$ $\frac{P_6}{P_{24}} = 52\%$
 - (c) Adjusted $P_6^{(2)} = 3.5$
- (d) t_x = ____ min
- (e) I = in./hr.

Note: This chart replaces the Intensity-Duration-Frequency curves used since 1965.

| Pe | - | 5 | ~ | 2.5 | e | 3,5 | 4 | 4.5 | s | 5.5 | 9 |
|----------|----------|------|------|---------------|--------|------|-------|-------|-------|-------|-------|
| Ouration | - | _ | - | | | | | - | _ | - | - |
| w | ત્રં | | 5.27 | 6.59 | | 9.22 | 10.54 | 11.86 | 13.17 | 14 49 | 15.81 |
| _ | 2.12 | | | 5.30 | | 7.42 | 8,48 | - | 10.60 | 11 66 | |
| 9 | | 2.53 | 3.37 | 4.21 | 5.05 | 5.90 | 6.74 | 7.58 | 8.42 | 9.27 | 0 |
| 5 | - | - | 2.59 | (C) | 8 | | 5.19 | 5.84 | 6.49 | 7.13 | 7.78 |
| 8 | 1.08 | 1.62 | 2.15 | N | · marc | | 4.3 | 4.85 | 5.39 | 5.93 | 6.46 |
| 52 | 0.93 | 1.40 | 1.87 | ťΛ | ςi | 3.27 | 3.73 | 4.20 | 4.67 | 5.13 | 5.60 |
| ၕ | 0.83 | 1.24 | 1.66 | €/I | c, | 5.80 | 3.32 | 3.73 | 4.15 | 4.56 | 4 98 |
| \$ | 0.69 | 1,93 | 138 | | N | 241 | 2.76 | 3.10 | 3.45 | 3.79 | 4. |
| SS | 0.60 | 0.90 | 1.19 | *** | - | 2.09 | 2.39 | 2.69 | 2.98 | 3.28 | 3.58 |
| 8 | 0.53 | 0.80 | 8 | - | 1.59 | 1.86 | 2.12 | 2.39 | 2.65 | 2 92 | 3 18 |
| 8 | 0.43 | 0.61 | 0.83 | <u>,</u> 용 | 1.23 | 43 | 1.63 | 1.84 | 58 | 2.25 | 2 45 |
| 22 | <u>8</u> | 0.51 | 0.68 | | | 1.13 | 38. | 1,53 | 22 | 1.87 | 204 |
| 55 | 0.29 | 0.44 | 0.59 | 0.73 | 0.88 | 5 | 1.18 | 1.32 | 1.47 | 1.62 | 2/2 |
| 180 | 0.26 | 0.39 | 0.52 | 0.65 | 0.78 | 0.91 | 2 | | 1.31 | 4 | 1.57 |
| 240 | 0.22 | 0.33 | 0.43 | 0.54 | | 0.76 | 0.87 | 0.98 | 8 | ç | S |
| 36 | 0.19 | 0.28 | 0.38 | 0.47 | | 99.0 | 0.75 | 0.85 | 0.94 | 1.03 | 3 2 |
| 360 | 0.17 | 0.25 | 0.33 | 0.42 | | | | 0.75 | D 8.4 | 8 | 8 |

FIGUR

San Diego County Hydrology Manual Date: June 2003

3 6 of 26 Section: Page:

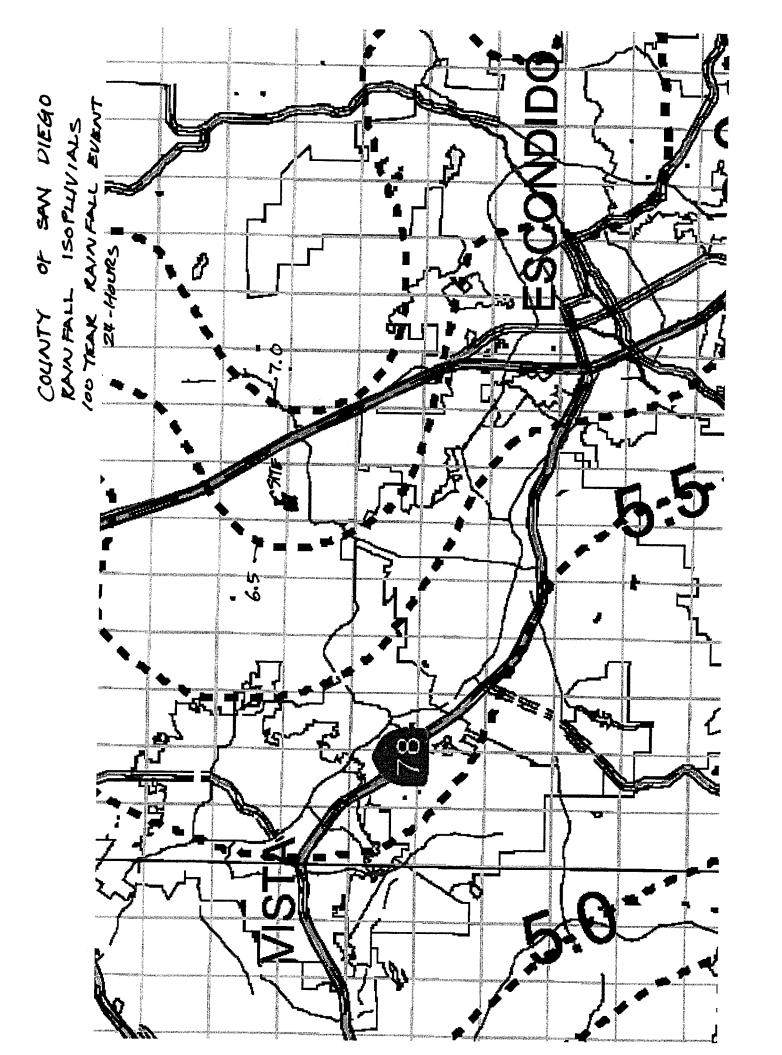
Table 3-1 RUNOFF COEFFICIENTS FOR URBAN AREAS

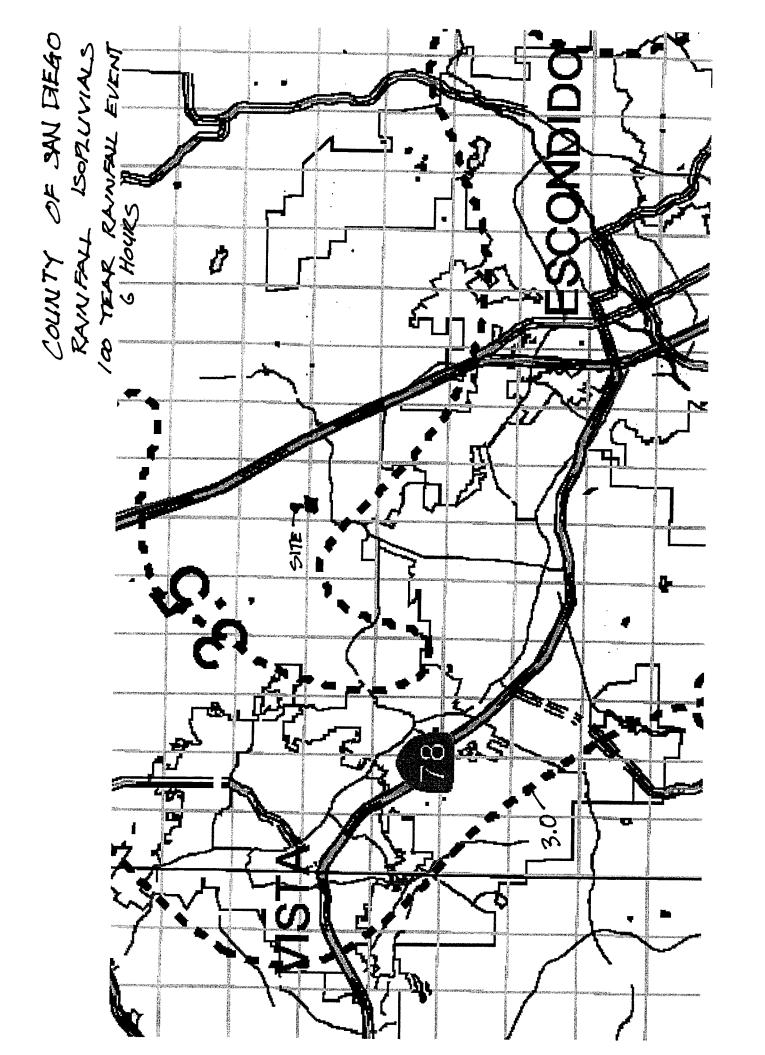
| La | Land Use | | D | D (1.0.) | , | |
|---------------------------------------|--------------------------------|----------|------|----------|-----------|------|
| | | | myr | Soil | Soil Type | |
| NRCS Elements | County Elements | % IMPER. | A | B | C | Q |
| Undisturbed Natural Terrain (Natural) | Permanent Open Space | *0 | 0.20 | 0.25 | 0:30 | 0.35 |
| Low Density Residential (LDR) | Residential, 1.0 DU/A or less | 10 | 0.27 | 0.32 | 0.36 | 0.41 |
| Low Density Residential (LDR) | Residential, 2.0 DU/A or less | 20 | 0.34 | 0.38 | 0.42 | 0.46 |
| Low Density Residential (LDR) | Residential, 2.9 DU/A or less | 25 | 0.38 | 0.41 | 0.45 | 0.49 |
| Medium Density Residential (MDR) | Residential, 4.3 DU/A or less | 30 | 0.41 | 0.45 | 0.48 | 0.52 |
| Medium Density Residential (MDR) | Residential, 7.3 DU/A or less | 40 | 0.48 | 0.51 | 0.54 | 0.57 |
| Medium Density Residential (MDR) | Residential, 10.9 DU/A or less | 45 | 0.52 | 0.54 | 0.57 | 09.0 |
| Medium Density Residential (MDR) | Residential, 14.5 DU/A or less | 50 | 0.55 | 0.58 | 0.60 | 0.63 |
| High Density Residential (HDR) | Residential, 24.0 DU/A or less | 65 | 99.0 | 0.67 | 69.0 | 0.71 |
| High Density Residential (HDR) | Residential, 43.0 DU/A or less | 08 | 97.0 | 0.77 | 0.78 | 0.79 |
| Commercial/Industrial (N. Com) | Neighborhood Commercial | 80 | 97.0 | 0.77 | 0.78 | 0.79 |
| Commercial/Industrial (G. Com) | General Commercial | 85 | 080 | 080 | 0.81 | 0.82 |
| Commercial/Industrial (O.P. Com) | Office Professional/Commercial | 06 | 0.83 | 0.84 | 0.84 | 0.85 |
| Commercial/Industrial (Limited I.) | Limited Industrial | 06 | 0.83 | 0.84 | 0.84 | 0.85 |
| Commercial/Industrial (General I.) | General Industrial | 95 | 0.87 | 0.87 | 0.87 | 0.87 |
| | | | | | | |

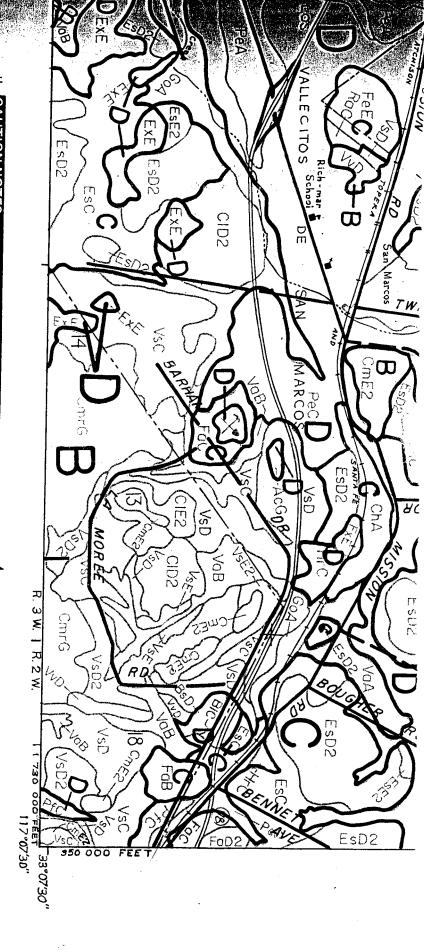
^{*}The values associated with 0% impervious may be used for direct calculation of the runoff coefficient as described in Section 3.1.2 (representing the pervious runoff coefficient, Cp, for the soil type), or for areas that will remain undisturbed in perpetuity. Justification must be given that the area will remain natural forever (e.g., the area is located in Cleveland National Forest).

DU/A = dwelling units per acre

NRCS = National Resources Conservation Service







CAUTION NOTES:

criteria, map sources, additional legend items, and necessary explanation of ratings shown on map. User is urged to refer to corresponding SUP PLEMENTAL DATA SHEET for assumptions.

2. This map does not eliminate the need for detailed on-site investigation of the soil and site to determine precise soil conditions prior to underother soils related activity. taking any construction, grading, planting, 9

Runoff

Base Map Source: U. S. Geological Survey with California State Coordinate System, Zone 6 Indicated

Prepared by: U. S. Department of Agriculture, Soil Conservation Service

Published by: San Diego County Planning Department for the Comprehensive Planning Organization — 1969



¼ mile 2000 SCALE 1:24000 1/2 mile 4000

6000 feet

1 mile

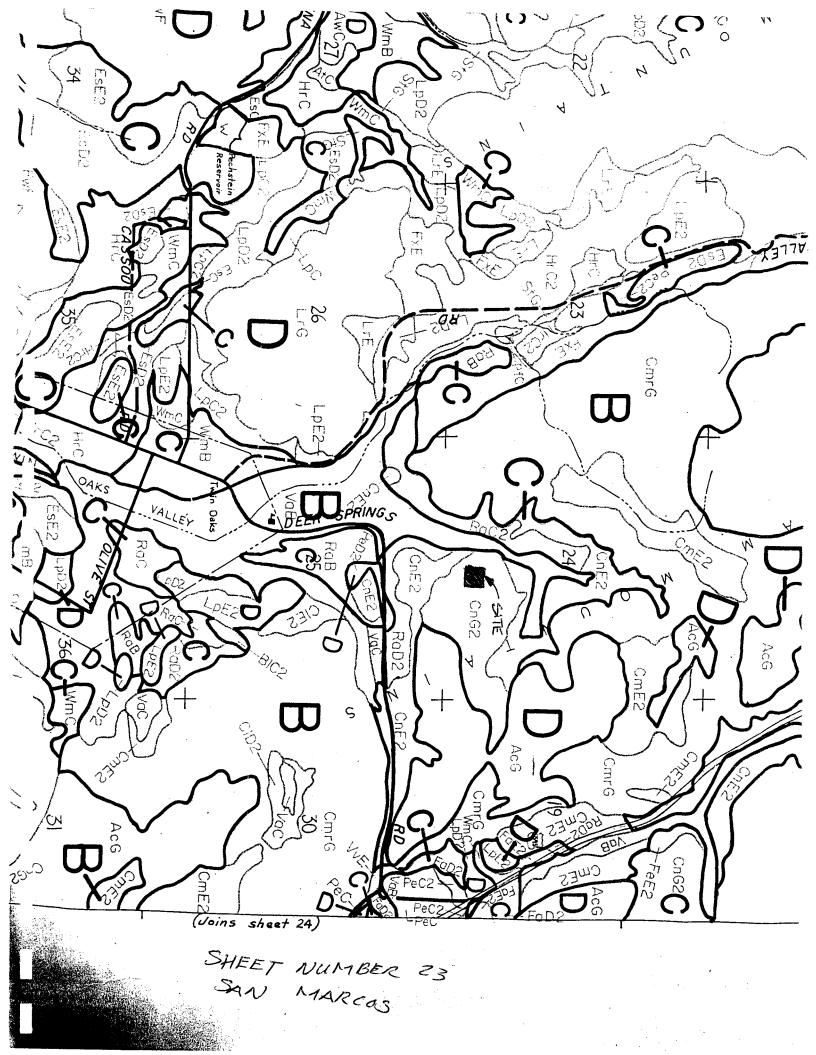
FEDERAL ASSISTANCE — The preparation of this map was financed in part through a comprehensive planning grant from the Department of Housing and Urban Development.



San Marcos

SHEET NAME

23

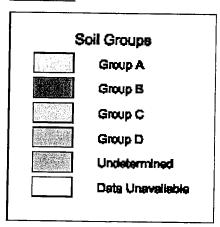


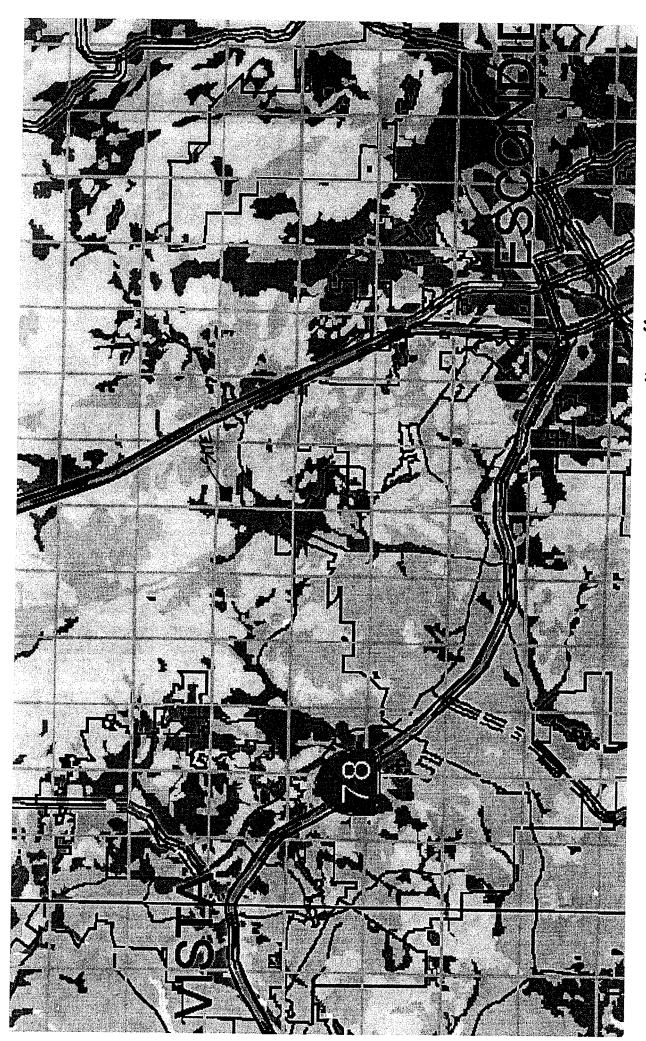
County of San Diego Hydrology Manual



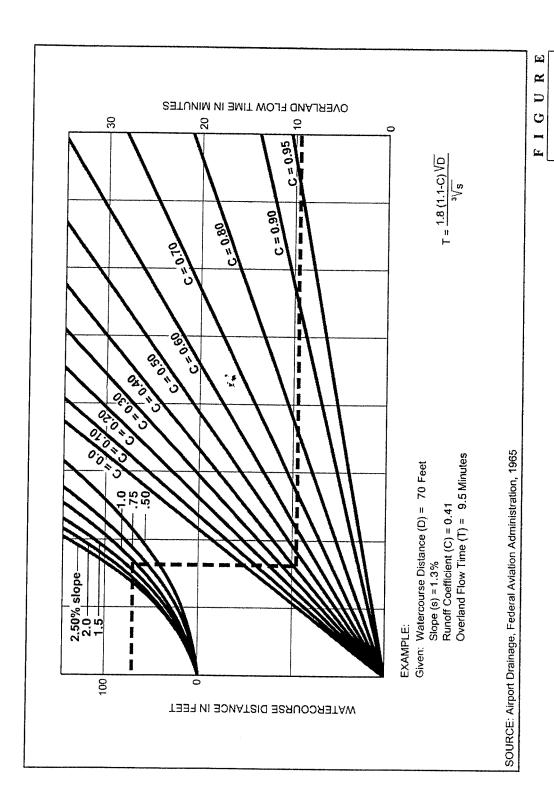
Soil Hydrologic Groups

Legend





2017 dhoah "C"



Rational Formula - Overland Time of Flow Nomograph

| San Diego County Hydrology Manual | Section: | 3 |
|-----------------------------------|----------|----------|
| Date: June 2003 | Page: | 12 of 26 |
| | | |

Note that the Initial Time of Concentration should be reflective of the general land-use at the upstream end of a drainage basin. A single lot with an area of two or less acres does not have a significant effect where the drainage basin area is 20 to 600 acres.

Table 3-2 provides limits of the length (Maximum Length (L_M)) of sheet flow to be used in hydrology studies. Initial T_i values based on average C values for the Land Use Element are also included. These values can be used in planning and design applications as described below. Exceptions may be approved by the "Regulating Agency" when submitted with a detailed study.

MAXIMUM OVERLAND FLOW LENGTH (L_M) & INITIAL TIME OF CONCENTRATION (T.)

Table 3-2

| | C INTIAL TIME OF CONCENTRATION (Ii) | | | | | | | | | | | | |
|------------|-------------------------------------|----------------|---------|----------------|------|----------------|------|----------------|---------|----------------|---------|---------|---------|
| Element* | DU/ | | 5% | 1 | % | 2 | 2% | 3 | % | 5 | % | 10 | 1% |
| | Acre | L _M | T_{i} | L _M | Ti | L _M | Ti | L _M | T_{i} | L _M | T_{i} | L_{M} | T_{i} |
| Natural | | 50 | 13.2 | 70 | 12.5 | 85 | 10.9 | 100 | 10.3 | 100 | 8.7 | 100 | 6.9 |
| LDR | 1 | 50 | 12.2 | 70 | 11.5 | 85 | 10.0 | 100 | 9.5 | 100 | 8.0 | 100 | 6.4 |
| LDR | 2 | 50 | 11.3 | 70 | 10.5 | 85 | 9.2 | 100 | 8.8 | 100 | 7.4 | 100 | 5.8 |
| LDR | 2.9 | 50 | 10.7 | 70 | 10.0 | 85 | 8.8 | 95 | 8.1 | 100 | 7.0 | 100 | 5.6 |
| MDR | 4.3 | 50 | 10.2 | 70 | 9.6 | 80 | 8.1 | 95 | 7.8 | 100 | 6.7 | 100 | 5.3 |
| MDR | 7.3 | 50 | 9.2 | 65 | 8.4 | 80 | 7.4 | 95 | 7.0 | 100 | 6.0 | 100 | 4.8 |
| MDR | 10.9 | 50 | 8.7 | 65 | 7.9 | 80 | 6.9 | 90 | 6.4 | 100 | 5.7 | 100 | 4.5 |
| MDR | 14.5 | 50 | 8.2 | 65 | 7.4 | 80 | 6.5 | 90 | 6.0 | 100 | 5.4 | 100 | 4.3 |
| HDR | 24 | 50 | 6.7 | 65 | 6.1 | 75 | 5.1 | 90 | 4.9 | 95 | 4.3 | 100 | 3.5 |
| HDR | 43 | 50 | 5.3 | 65 | 4.7 | 75 | 4.0 | 85 | 3.8 | 95 | 3.4 | 100 | 2.7 |
| N. Com | | 50 | 5.3 | 60 | 4.5 | _75 | 4.0 | 85 | 3.8 | 95 | 3.4 | 100 | 2.7 |
| G. Com | | 50 | 4.7 | 60 | 4.1 | 75 | 3.6 | 85 | 3.4 | 90 | 2.9 | 100 | 2.4 |
| O.P./Com | | 50 | 4.2 | 60 | 3.7 | 70 | 3.1 | 80 | 2.9 | 90 | 2.6 | 100 | 2.2 |
| Limited I. | | 50 | 4.2 | 60 | 3.7 | 70 | 3.1 | 80 | 2.9 | 90 | 2.6 | 100 | 2.2 |
| General I. | | 50 | 3.7 | 60 | 3.2 | 70 | 2.7 | 80 | 2.6 | 90 | 2.3 | 100 | 1.9 |

^{*}See Table 3-1 for more detailed description

TABLE - 15

INTERPRETATIONS FOR LAND MANAGEMENT

KEY TO INTERPRETATION RATING SYMBOLS:

HYDROLOGIC SOIL GROUPS:

LIMITATIONS:

A - HIGH INFILTRATION RATE

SL - SLIGHT DEGREE OF LIMITATION B - MODERATE INFILTRATION RATE
C - SLOW INFILTRATION RATE
D - VERY SLOW INFILTRATION RATE

SL - SLIGHT DEGREE OF LIMITATION
M - MODERATE DEGREE OF LIMITATION
SE - SEVERE DEGREE OF LIMITATION

| | ~~~ | TETT SEGNTAFIETHAT | TON HATE | | | | |
|---|---|---|--|---|---------------------|----------------------------|--|
| | | Interpretation Rating | | | | Interpretation Rating | ь |
| Soil Map Symbol ^a | Hydrologic Group | Erodibility by Water | Conversion from Brush to Grass | Soil Map Symbol ^a | Hydrologic Group | Erodibility by Water | Conversion from Brush to Grass |
| (1) | (2) | (3) | (4) | (1) | (2) | (3) | (4) |
| CmrG | В | SE (slp) | SE | FaC | C | SE (str) | SL |
| CnE2 c (CI) (Fa) (CnG2 c (CI) (Fa) Co Cr CsB CsC CsD CtE CtF CuE CuG CvG DaC DaD DaE DaE2 DaF DcD c (Da) (Ur) DcF c (Da) (Ur) DoE c (Da) (Ur) DoE c (Da) (Oh) | B C D A A A B B B B D D D D D D D D D D D D | SE (str) SE (slp) SE (slp) M (txt) SE (txt) SE (txt) SE (str) SE (slp) SE (slp) SE (slp) SE (slp) SL SL M (slp) SE (slp) M (slp) SE (slp) M (slp) M (slp) M (slp) M (slp) M (slp) | SE SE SE SE SL SL SL SL SL SL M M M M M SL | FaC2 FaD2 FaE2 FaE3 FeC FeE FeE2 FvD c (Fa) (Vs) FvE c (Fa) (Vs) FwF FxE FxG GaE GaF GoA GrA GrB GrC GrD HaG HmD HmE HnE HnG HoC HrC HrC2 | C | SE (str) | SL SL SL SL SL SL M M M SL M SE SE SE SE SE SL |
| EdC EsC EsD2 EsE2 EvC ExE ExG | B C C C D D D | M (txt) SE (str) SE (str) SE (str) SE (str) SE (str) SE (str) SE (dpt) SE (slp) | SL SL SL SL SL SE SE | HrD HrD2 HrE2 HuC ° (Hr) (Ur) HuE ° (Hr) | D D D | SE (dpt) SE (dpt) SE (dpt) | SL SL SL |
| FaB | С | SE (str) | SL | (Ur) | | | |



IER CP

LAND USE ELEMENT

| 2 8 9 | 6 | (2) | (2) | 24 | 26 | | |
|---|--|--|-------------------------------------|---|-----------------------------|----------------------------|-----------------------------|
| | | | | | | | |
| MULTIPLE RURAL USE 1 Dwelling Unit/4, 8, 20 Acres | INTENSIVE AGRICULTURE 1 Dwelling Unit/2, 4 & 8 Acres | AGRICULTURAL PRESERVES 1 Dwelling Unit/8 Acres | SPECIFIC PLAN AREA | IMPACT SENSITIVE AREA 1 Dwelling Unit/4, 8, 20 Acres | VISITOR, SERVING COMMERCIAL | | EGEND Intermittent Drainage |
| 18 | 19 | 20 | 21 (| 24 | 56 | | Local Roads |
| | | | | | | | |
| | $\bigcirc 2$ | | 9 | $\begin{array}{c} \\ \\ \\ \\ \\ \end{array}$ | 15 | $\bigcirc 11)$ | |
| TIAL 1, 2 & 4 Acres | ITIAL Jnit/Acre | ITIAL Jnits/Acre | ITIAL Jnits/Acre | MMERCIAL | USTRIAL | TE 2 & 4 Acres | Freeways |
| RESIDENTIA | RESIDENTI/ | RESIDENTIAL 2.0 Dwelling Units/Acre | RESIDENTIAL 7.3 Dwelling Units/Acre | GENERAL COMM | LIMITED INDUSTRIA | ESTATE 1 Dwelling Unit/2 & | |
| | | | | | | | |
| (-) | (5) | က | 9 | (E) | 15 | [1] | |
| \bigcirc | | | | | | | |
| | | | | | | , | |
| | | | | | | | |

Property Lines

Contours

Sub Local Roads

Prime Arterials

Maior Roads

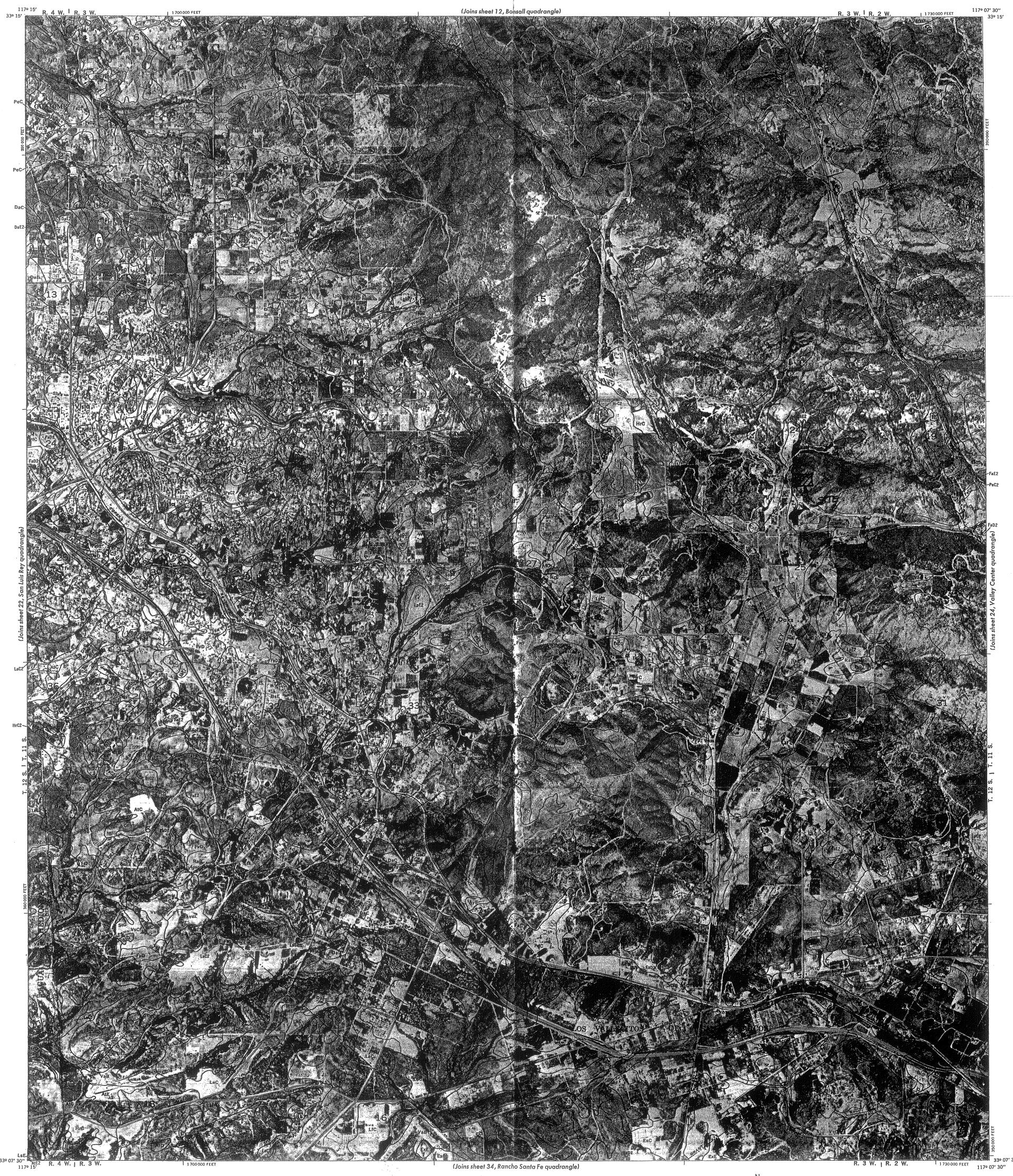
Trails

LAND USE ELEMENT

| | | | | | ESTATE 1 Dwelling Unit/2 & 4 Acres | |
|----------------------------------|---------------|--------------------------------|----------------|--------------|------------------------------------|---------------|
| | 7 | | 07 | <u> </u> | LIMITED INDOSTRIAL | |
| ilod | 96 | 7,0,'+/1110 gringary 1 | | | | ! |
| und und | | | | 2 | | ر 2 |
| Sph Sph 7 7 | 74) | IMPACT SENSITIVE AREA | 74 | | GENERAL COMMERCIAL | 2 |
| | | |) (| | 7.3 Dwelling Units/Acre | |
| areas are ad 2. ONE ACR | \mathcal{I} | SPECIFIC PLAN AREA | (21 | 9 | RESIDENTIAL | 9 |
| and do no. Only the a | | 1 Dwelling Unit/8 Acres | | | 2.0 Dwelling Units/Acre | |
| NOTES: 1. PROPERT) | $\supset 20$ | AGRICULTURAL PRESERVES | $) \qquad (20$ | (L) | RESIDENTIAL | \mathcal{C} |
| COUNTRY TOWN B | | 1 Dwelling Unit/2, 4 & 8 Acres | | | 1.0 Dwelling Unit/Acre | |
| ESCONDIDO SPHÉRE INFLUENCE BOUND | ○ 19 | INTENSIVE AGRICULTURE | (19 | \bigcirc 2 | RESIDENTIAL | 5 |
| DEVELOPMENT BOU | | 1 Dwelling Unit/4, 8, 20 Acres |) | | 1.0 Dwelling Unit/1,2 & 4 Acres | |
| ALL STREETS SHOW | 0 18 | MULTIPLE RURAL USE | 18 | | RESIDENTIAL | |
| HOLIO OFFICERO | | | | | | |

NORTH COL * Sturly Area Boundary Intermittent Drainage Property Lines Contours 000 000 000 000 000 000 000 000 LEGEND Sub Local Roads Local Roads Sortion List Trails מלביה חייונים ה Prime Arterials Major Roads Freeways

(Joins sheet 12, Bonsall quadrangle)



Soil Survey by USDA, Soil Conservation Service in cooperation with the University of California Agricultural Experiment Station. Photobase compiled 1970 from 1967-68 aerial photography. Control from USGS and USC & GS.

Polyconic projection. 1927 North American datum. 10,000-foot grid based on California plane coordinate system, zone 6.

Land division corners are approximate.

Scale 1:24 000

This map is one of a set of 76 compiled 1969-70 by the Soil Conservation Service. SAN DIEGO AREA, CALIFORNIA NO. 23

Cooperating Agencies San Diego County Planning Department
San Diego County Comprehensive Planning Organization U.S. Dept. of Agriculture-Forest Service U.S. Dept. of the Interior-Bureau of Indian Affairs Dept. of the Navy-U.S. Marine Corps

NORTH COUNTY METRO SRA SHEET 4